

Section 4: Reference Frames and Transformations

Much of robotics deals with manipulating objects or moving through space. Therefore it is necessary that we develop the tools necessary to describe positions and rotations. A *reference frame* is a coordinate system in which a particular quantity is expressed. Reference frames can be fixed to some point in space, or they can be moving and rotating.

The Universal Reference Frame F_U

We assume that every robotic system always has some *universal reference frame* that is not moving or rotating, we call this reference frame F_U . For example, the position of an object in this reference frame can be denoted by a vector such as

$$(\mathbf{r})_U = \begin{pmatrix} (r_x)_U \\ (r_y)_U \\ (r_z)_U \end{pmatrix}$$

In this course, we will use rounded brackets preceded by a subscript to denote the reference frame in which a vector is expressed. In the above example $(\mathbf{r})_U$ indicates that the vector \mathbf{r} is numerically expressed in the F_U frame. The moment we assign specific values to \mathbf{r} it is implicitly assumed that we have chosen a particular reference frame. Since we will be dealing with many different coordinate frames this notation will help clarify in which frame the vector is expressed. Although we mention a position vector above, numerous other vector quantities are used in robotics (e.g., to represent forces, torques, velocities).

Numerically Expressing Vectors

Consider a two-dimensional vector \mathbf{r} and the three reference frames in Fig. 1. These three frames might represent, for example, snapshots of a single frame that is rigidly attached to a rotating object. The vector \mathbf{r} does not change in each case, but in each reference frame \mathbf{r} is represented by a different set of numeric values. For example, in the frame F_A the vector \mathbf{r} is numerically represented by

$$(\mathbf{r})_A = \begin{pmatrix} (r_x)_A \\ (r_y)_A \end{pmatrix}$$

The number $(r_x)_A$ represents the projection of the vector \mathbf{r}_A onto the $\hat{\mathbf{x}}_A$ axis. Similarly, the numeric values of \mathbf{r}_B and \mathbf{r}_C will be different since their axes are different.

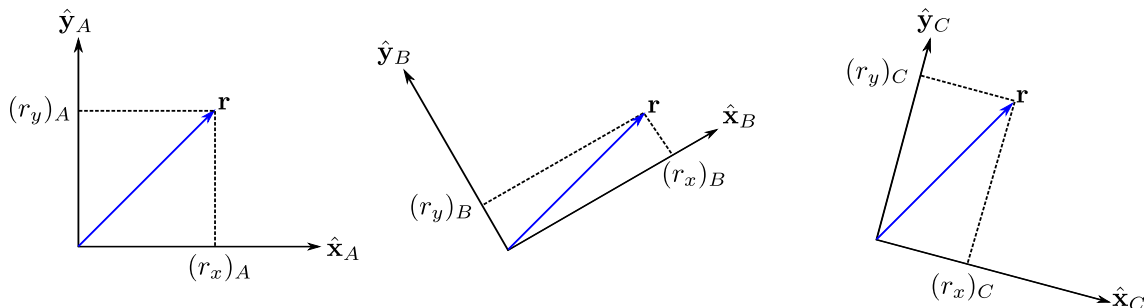


Figure 1: The vector \mathbf{r} in three reference frames: F_A , F_B and F_C . Note that the numeric representation of the vector will be different in each frame, even though the vector remains unchanged.

Side Note: Projecting Vectors and the Dot Product

For vectors \mathbf{v}_1 and \mathbf{v}_2 , the projection of \mathbf{v}_1 onto \mathbf{v}_2 (or vice versa) is the dot product

$$\mathbf{v}_1 \cdot \mathbf{v}_2 = \|\mathbf{v}_1\| \|\mathbf{v}_2\| \cos \theta \quad (1)$$

where θ is the angle between \mathbf{v}_1 and \mathbf{v}_2 . In the example above, the value $(r_x)_A$ represents the projection of the \mathbf{r} vector onto the $\hat{\mathbf{x}}_A$ unit vector, in other words: $(r_x)_A = \mathbf{r} \cdot \hat{\mathbf{x}}_A$

Common Reference Frames

A *Cartesian* reference frame F_A consists of the unit vectors $\hat{\mathbf{x}}_A$, $\hat{\mathbf{y}}_A$ and $\hat{\mathbf{z}}_A$ corresponding to three perpendicular planes (see Fig. 2a). In the F_A frame itself these are all vectors with all zeros entries and one entry equal to one, in three dimensions:

$$(\hat{\mathbf{x}}_A)_A = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \quad (\hat{\mathbf{y}}_A)_A = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} \quad (\hat{\mathbf{z}}_A)_A = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \quad (2)$$

However, these unit vectors can also be expressed in a different reference frame. For example, if there is some other reference frame F_B , these unit vectors will take on other numeric values and will be denoted $(\hat{\mathbf{x}}_A)_B$, $(\hat{\mathbf{y}}_A)_B$ and $(\hat{\mathbf{z}}_A)_B$. (We will return to this point later.)

In this course we will mainly use a Cartesian reference frame, but other non-Cartesian coordinate systems are also possible: such as *spherical* or *cylindrical* coordinates (Figs. 2b and 2c). The choice of reference frame depends on the problem at hand; although the Cartesian frame is the natural first choice, sometimes using a spherical or cylindrical system can make the problem much simpler.

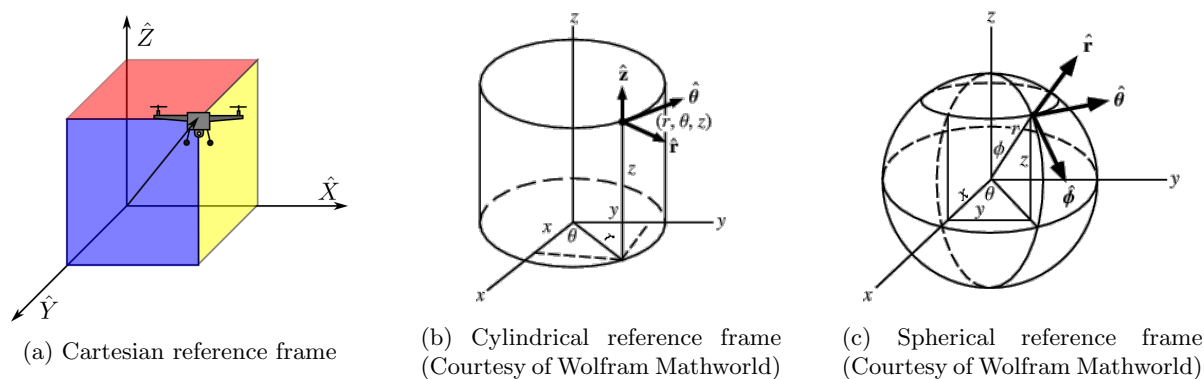


Figure 2: Common reference frames

Side Note: Vector and Matrix Notation

In this course we will use the following conventions:

- plain text denotes scalars (e.g., v)
- lower case bold type denotes vectors (e.g., \mathbf{v})
- unit vectors will be denoted with a $\hat{}$ symbol (e.g., $\hat{\mathbf{x}}$)

- the transpose of a vector is denoted with a superscript T symbol

e.g., if $\mathbf{v} = \begin{pmatrix} v_1 \\ v_2 \\ \vdots \\ v_n \end{pmatrix}$ then $\mathbf{v} = (v_1 \ v_2 \ \cdots \ v_n)^T$ and $\mathbf{v}^T = (v_1 \ v_2 \ \cdots \ v_n)$

- upper case bold type denotes matrices (e.g., \mathbf{V})
- when we say a matrix \mathbf{A} is an $m \times n$ matrix it implies that \mathbf{A} has m rows and n columns

- the matrix transpose is denoted with the superscript T symbol

e.g., if $\mathbf{A} = \begin{pmatrix} a & b & c \\ d & e & f \\ g & h & i \end{pmatrix}$ then $\mathbf{A}^T = \begin{pmatrix} a & d & g \\ b & e & h \\ c & f & i \end{pmatrix}$

- a square identity matrix with n rows and n columns is denoted by $\mathbf{1}_{n \times n} = \begin{pmatrix} 1 & 0 & \cdots & 0 \\ 0 & 1 & \cdots & \vdots \\ \vdots & \cdots & \ddots & \vdots \\ 0 & \cdots & \cdots & 1 \end{pmatrix}$

- multiplying a vector or matrix by the identity matrix leaves the vector or matrix unchanged

e.g. $\mathbf{1}_{n \times n} \mathbf{v} = \mathbf{v}$ or $\mathbf{1}_{n \times n} \mathbf{A} = \mathbf{A}$

- the inverse of a matrix is denoted \mathbf{A}^{-1}

- Fact: if \mathbf{A} is a square $n \times n$ matrix then $\mathbf{A}\mathbf{A}^{-1} = \mathbf{A}^{-1}\mathbf{A} = \mathbf{1}_{n \times n}$ and the matrices “cancel”

- An example equation that illustrates some of this notation is the eigenvalue equation: $\lambda \mathbf{v} = \mathbf{A}\mathbf{v}$ which includes a scalar eigenvalue λ , an eigenvector \mathbf{v} , and a matrix \mathbf{A} .

A Motivating Problem

Consider the robotic arm shown in Fig. 3. A rotating camera is attached at the end of the arm. The vector \mathbf{p}_c describes where the camera is located with respect to the origin of the F_U frame. Suppose that

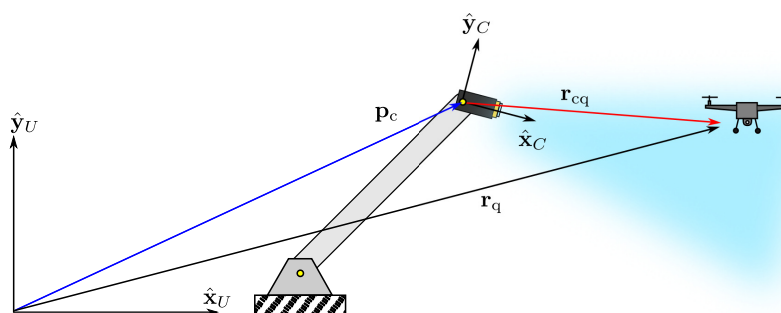


Figure 3: The position and orientation of a planar robotic arm

the position of quadcopter relative to the camera is \mathbf{r}_{cq} . Thus the position of the quadcopter relative to the origin of the F_U frame is

$$\mathbf{r}_q = \mathbf{p}_c + \mathbf{r}_{cq} \quad (3)$$

To carry out the computation, and obtain numeric values for \mathbf{r}_q , we must choose a consistent reference frame in which to express each of the three vectors in Eq. 3. A natural choice is to use the F_U reference frame. Thus we can re-write Eq. 3 as

$$(\mathbf{r}_q)_U = (\mathbf{p}_c)_U + (\mathbf{r}_{cq})_U \quad (4)$$

to emphasize that all of the vectors being added are expressed in the F_U frame. Suppose we already have \mathbf{p}_c in the F_U frame (i.e., we have $(\mathbf{p}_c)_U$), but the vector \mathbf{r}_{cq} is given in the F_C frame as $(\mathbf{r}_{cq})_A$. This is a very common situation. For example, the F_C frame might represent the direction in which the camera is pointed and a machine vision algorithm that uses the camera images might output relative position vectors of objects it detects in this frame only. It is clear that we need a way to convert a vector in the frame F_C to a vector in the frame F_U so that we can carry out computations such as the one in Eq. 4. As we will see in the following section, the enabling tool is a *rotation matrix*.

2D Rotation Matrices

Besides knowing the position of an object we are often interested in the orientation of it. A common way to describe the orientation of a rigid body is to attach a fixed reference frame to it. This body-attached reference frame is not necessarily used to express any other vectors – *the reference frame itself expresses the orientation of the rigid body*. One way to relate two reference frames, F_A and F_B , is to express the unit vectors of the F_B reference frame using the F_A frame (i.e., to express $(\hat{\mathbf{x}}_B)_A$, $(\hat{\mathbf{y}}_B)_A$ and $(\hat{\mathbf{z}}_B)_A$). Then by assembling these vectors as columns of a new matrix we obtain a rotation matrix \mathbf{R}_B^A which can be used to convert vectors from one frame to the other, and vice versa. The following example will illustrate this concept for a two-dimensional reference frame. Consider the two reference frames in

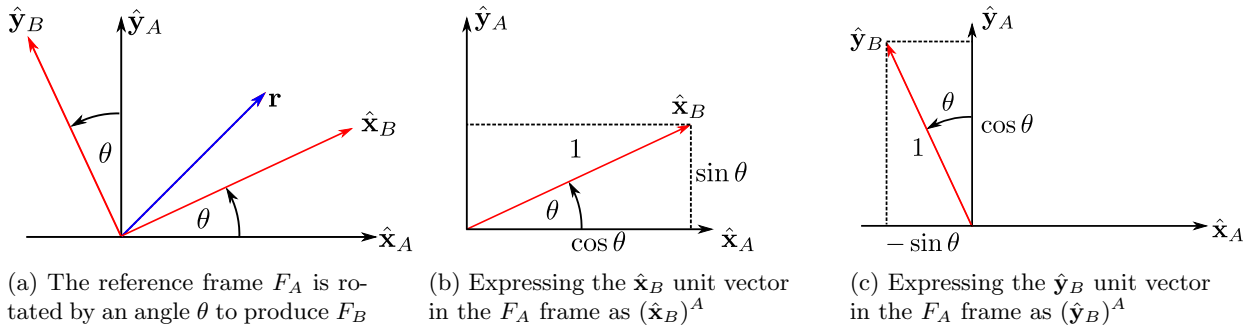


Figure 4: A 2D passive rotation.

Fig. 4a. The vector \mathbf{r} can be represented as either $(\mathbf{r})_A$ or $(\mathbf{r})_B$. The unit vectors $\hat{\mathbf{x}}_B$ and $\hat{\mathbf{y}}_B$ have a length of one (by definition) thus $\|(\hat{\mathbf{x}}_B)_A\| = \|(\hat{\mathbf{y}}_B)_A\| = 1$. To express the unit vectors of the F_B frame in the F_A frame we need to find the projection of each unit vector onto the $\hat{\mathbf{x}}_A$ and $\hat{\mathbf{y}}_A$ axes. Using Eq. 1 we have:

$$\begin{aligned} \hat{\mathbf{x}}_B \cdot \hat{\mathbf{x}}_A &= \cos \theta \\ \hat{\mathbf{x}}_B \cdot \hat{\mathbf{y}}_A &= \cos(\pi/2 - \theta) = \sin \theta \\ \hat{\mathbf{y}}_B \cdot \hat{\mathbf{x}}_A &= \cos(\pi/2 + \theta) = -\sin \theta \\ \hat{\mathbf{y}}_B \cdot \hat{\mathbf{y}}_A &= \cos \theta \end{aligned}$$

where the angle argument of the cosine was determined by inspecting Fig. 4 for each case. Alternately, we could have arrived at the same results using trigonometry.

Regardless of the approach used, we obtain

$$(\hat{\mathbf{x}}_B)_A = \begin{pmatrix} \hat{\mathbf{x}}_B \cdot \hat{\mathbf{x}}_A \\ \hat{\mathbf{y}}_B \cdot \hat{\mathbf{y}}_A \end{pmatrix} = \begin{pmatrix} \cos \theta \\ \sin \theta \end{pmatrix} \quad \text{and} \quad (\hat{\mathbf{y}}_B)_A = \begin{pmatrix} \hat{\mathbf{y}}_B \cdot \hat{\mathbf{x}}_A \\ \hat{\mathbf{y}}_B \cdot \hat{\mathbf{y}}_A \end{pmatrix} = \begin{pmatrix} -\sin \theta \\ \cos \theta \end{pmatrix} \quad (5)$$

The rotation matrix can be constructed by using the vectors in (5) as the columns of the new matrix:

$$\mathbf{R}_B^A(\theta) = ((\hat{\mathbf{x}}_B)_A \quad (\hat{\mathbf{y}}_B)_A) = \begin{pmatrix} \hat{\mathbf{x}}_B \cdot \hat{\mathbf{x}}_A & \hat{\mathbf{y}}_B \cdot \hat{\mathbf{x}}_A \\ \hat{\mathbf{x}}_B \cdot \hat{\mathbf{y}}_A & \hat{\mathbf{y}}_B \cdot \hat{\mathbf{y}}_A \end{pmatrix} = \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix} \quad (6)$$

When we multiply a vector $(\mathbf{v})_B$ by this matrix we obtain the desired result:

$$(\mathbf{v})_A = \mathbf{R}_B^A(\theta)(\mathbf{v})_B \quad (7)$$

The rotation matrix \mathbf{R}_B^A has subscript B and superscript A to denote that it converts vectors from the frame F_B to F_A . To convince yourself that Eq. 7 indeed converts vectors as claimed, consider what happens when we pre-multiply the unit vectors $\hat{\mathbf{x}}_B$ and $\hat{\mathbf{y}}_B$, expressed in the F_B frame, by the rotation matrix – we obtain:

$$\mathbf{R}_B^A(\theta)(\hat{\mathbf{x}}_B)_B = \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} 1 \\ 0 \end{pmatrix} = \begin{pmatrix} \cos \theta \\ \sin \theta \end{pmatrix} = (\hat{\mathbf{x}}_B)_A$$

and

$$\mathbf{R}_B^A(\theta)(\hat{\mathbf{y}}_B)_B = \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} 0 \\ 1 \end{pmatrix} = \begin{pmatrix} -\sin \theta \\ \cos \theta \end{pmatrix} = (\hat{\mathbf{y}}_B)_A$$

which are exactly the expressions in Eq. 5. Since any vector in the F_B frame is simply a linear combination of the unit vectors then clearly the same procedure applies.

The matrix (6) is parametrized by the angle θ thus we can use it as a general formula for any rotation of 2D reference frames. Note that θ is measured counter-clockwise from the $\hat{\mathbf{x}}_A$ axis to the $\hat{\mathbf{x}}_B$ axis which is, in general, *not from the horizontal*. (In the following we drop the reference to θ and assume that this is implied from context.) However, Eq. 7 can only convert vectors one way: from the F_B frame to the F_A frame. If Eq. 7 was a scalar equation we could obtain \mathbf{v}_B by dividing both sides by \mathbf{R}_B^A . But recall that matrix division is not possible – instead we must “invert” the matrix to obtain $(\mathbf{R}_B^A)^{-1}$ and pre-multiply both sides. The quantity $(\mathbf{R}_B^A)^{-1}(\mathbf{R}_B^A) = \mathbf{1}_{n \times n}$ is equal to the identity matrix (a n -by- n diagonal matrix of ones) and effectively “cancels” itself. Thus

$$\begin{aligned} (\mathbf{v})_A &= (\mathbf{R}_B^A)(\mathbf{v})_B \\ (\mathbf{R}_B^A)^{-1}(\mathbf{v})_A &= (\mathbf{R}_B^A)^{-1}(\mathbf{R}_B^A)(\mathbf{v})_B \\ (\mathbf{R}_B^A)^{-1}(\mathbf{v})_A &= \mathbf{1}_{n \times n}(\mathbf{v})_B \\ (\mathbf{R}_B^A)^{-1}(\mathbf{v})_A &= (\mathbf{v})_B \end{aligned}$$

Since $(\mathbf{R}_B^A)^{-1}$ converts vectors from the F_A frame to the F_B frame we denote it as $\mathbf{R}_A^B(\theta)$

$$\mathbf{R}_A^B = (\mathbf{R}_B^A)^{-1}$$

Thus we have the desired conversion, but it requires that we compute the matrix inverse $(\mathbf{R}_B^A)^{-1}$. For generic matrices this can be computed numerically but it is cumbersome to compute analytically. Alternately, we could obtain \mathbf{R}_B^A by repeating the same procedure we used to arrive at \mathbf{R}_A^B . This would

involve expressing the F_B frame unit vectors in the F_A frame. Upon closer inspection of Eq. 6 it turns out that we've already done this! Notice that the rows of Eq. 6 are the vectors

$$[(\hat{\mathbf{x}}_A)_B]^T = \begin{pmatrix} \hat{\mathbf{x}}_A \cdot \hat{\mathbf{x}}_B & \hat{\mathbf{x}}_A \cdot \hat{\mathbf{y}}_B \end{pmatrix} \quad \text{and} \quad [(\hat{\mathbf{y}}_A)_B]^T = \begin{pmatrix} \hat{\mathbf{y}}_A \cdot \hat{\mathbf{x}}_B & \hat{\mathbf{y}}_A \cdot \hat{\mathbf{y}}_B \end{pmatrix}$$

Therefore we can obtain \mathbf{R}_A^B from \mathbf{R}_B^A by simply transposing the rows into columns. In other words:

$$\boxed{\mathbf{R}_A^B = (\mathbf{R}_B^A)^{-1} = (\mathbf{R}_B^A)^T}$$

Note that the way θ is defined is the same in \mathbf{R}_A^B and \mathbf{R}_B^A . Be careful to clearly identify, for a given problem, what reference frame corresponds to F_A , what reference corresponds to F_B , and how θ is measured. Rotation matrices are a special case in which the transpose is equal to the inverse of the matrix (i.e., they are *orthogonal* matrices). To summarize, if frame F_B is rotated by an angle of θ relative to F_A we have the following two equations that convert vectors from one frame to another:

$$\boxed{(\mathbf{v})_A = \mathbf{R}_B^A (\mathbf{v})_B = \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix} (\mathbf{v})_B} \quad (8)$$

$$\boxed{(\mathbf{v})_B = \mathbf{R}_A^B (\mathbf{v})_A = \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix} (\mathbf{v})_A} \quad (9)$$

In Eqs. (8)-(9) the angle θ is defined counter-clockwise from the $\hat{\mathbf{x}}_A$ axis to the $\hat{\mathbf{x}}_B$ axis.

Example: 2D Rotation Matrices from F_A to F_B

Suppose that the vector \mathbf{r} given in the F_A frame (Fig. 5) is

$$(\mathbf{r})_A = \begin{pmatrix} (r_x)_A \\ (r_y)_A \end{pmatrix} = \begin{pmatrix} 3 \\ 3 \end{pmatrix}$$

Now suppose the frame F_B is at an angle relative to F_A (measured counter-clockwise from the $\hat{\mathbf{x}}_A$ axis

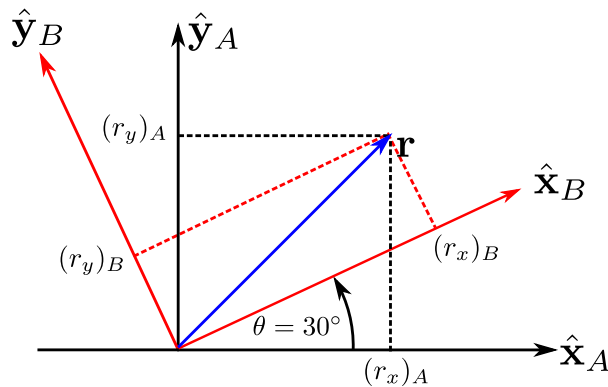


Figure 5: Rotating the \mathbf{r} vector from F_A to F_B

to the $\hat{\mathbf{x}}_B$ axis) of $\theta = 30^\circ$ relative to F_A . Then the rotation matrix that converts vectors from the F_A frame to the F_B frame can be evaluated as

$$\mathbf{R}_A^B|_{\theta=30^\circ} = \begin{pmatrix} \cos(30^\circ) & \sin(30^\circ) \\ -\sin(30^\circ) & \cos(30^\circ) \end{pmatrix} = \begin{pmatrix} 0.8660 & 0.5000 \\ -0.5000 & 0.8660 \end{pmatrix}$$

The vector \mathbf{r} in the F_B frame is then computed using Eq. 9

$$\begin{aligned} (\mathbf{r})_B &= \mathbf{R}_A^B(\mathbf{r})_A \\ &= \begin{pmatrix} 0.8660 & 0.5000 \\ -0.5000 & 0.8660 \end{pmatrix} \begin{pmatrix} 3 \\ 3 \end{pmatrix} \\ &= \begin{pmatrix} 4.098 \\ 1.098 \end{pmatrix} \end{aligned}$$

The fact that $(r_x)_B > (r_y)_A$ is consistent with Fig. 1 where it is clear that \mathbf{r}_B has a large component projected onto the unit vector $\hat{\mathbf{x}}_B$.

Example: 2D Rotation Matrices from F_B to F_A

Suppose that the vector \mathbf{r} given in the F_B frame (Fig. 5) is

$$(\mathbf{r})_B = \begin{pmatrix} (r_x)_B \\ (r_y)_B \end{pmatrix} = \begin{pmatrix} 0.5 \\ 0 \end{pmatrix}$$

Now suppose the frame F_B is at an angle relative to F_A (measured counter-clockwise from the $\hat{\mathbf{x}}_A$ axis

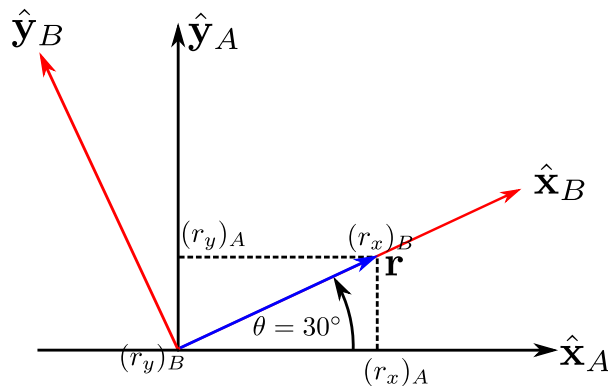


Figure 6: Rotating the \mathbf{r} vector from F_B to F_A

to the $\hat{\mathbf{x}}_B$ axis) of $\theta = 30^\circ$ relative to F_A . Then the rotation matrix that converts vectors from the F_B frame to the F_A frame can be evaluated as

$$\mathbf{R}_B^A|_{\theta=30^\circ} = \begin{pmatrix} \cos(30^\circ) & -\sin(30^\circ) \\ \sin(30^\circ) & \cos(30^\circ) \end{pmatrix} = \begin{pmatrix} 0.8660 & -0.5000 \\ 0.5000 & 0.8660 \end{pmatrix}$$

The vector \mathbf{r} in the F_B frame is then computed using Eq. 9

$$\begin{aligned} (\mathbf{r})_B &= \mathbf{R}_A^B(\mathbf{r})_A \\ &= \begin{pmatrix} 0.8660 & -0.5000 \\ 0.5000 & 0.8660 \end{pmatrix} \begin{pmatrix} 0.5 \\ 0 \end{pmatrix} \\ &= \begin{pmatrix} 0.433 \\ 0.250 \end{pmatrix} \end{aligned}$$

Reference frames won't always appear with the F_A axes pointing in the familiar left and up directions. Consider Fig. 7, in which the $\hat{\mathbf{x}}_A$ axis points up and the $\hat{\mathbf{y}}_A$ axis points to the left. The angle θ used in defining the rotation matrix is measured from $\hat{\mathbf{x}}_A$ axis to the $\hat{\mathbf{x}}_B$ axis – in this case that means the angle

can be written as negative.

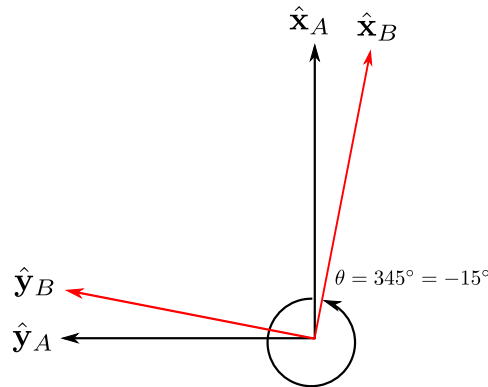


Figure 7: Atypical reference frame orientations

Rigid Transformations and Homogeneous Coordinates

In our discussion of 2D rotation matrices we learned how to express a vector in two different reference frames that were rotated relative to each other. This is applicable to vectors that have no spatial reference point or to convert between vectors that *shared a common origin*. We called each of these representations $(\mathbf{r})_A$ and $(\mathbf{r})_B$. Such *rotations* preserved the length of the vector (i.e., $\|(\mathbf{r})_A\| = \|(\mathbf{r})_B\|$).

Now we will discuss *rigid transformations* between reference frames. Rigid transformations are used to determine two vectors also called $(\mathbf{r})_A$ and $(\mathbf{r})_B$, each expressed in different reference frames, but that both *point to the same position in space*. It is a slight abuse of notation to call these vectors $(\mathbf{r})_A$ and $(\mathbf{r})_B$ since they are no longer the *same vector* as in the case of the rotation transformations above. Since the reference frame origins are not collocated the two vectors will not have the same length in general (i.e., $\|(\mathbf{r})_A\| \neq \|(\mathbf{r})_B\|$). This situation is illustrated in Fig. 8, both $(\mathbf{r})_A$ and $(\mathbf{r})_B$ point to the same position in space (point Q) but each originates from the origin of a different reference frame.

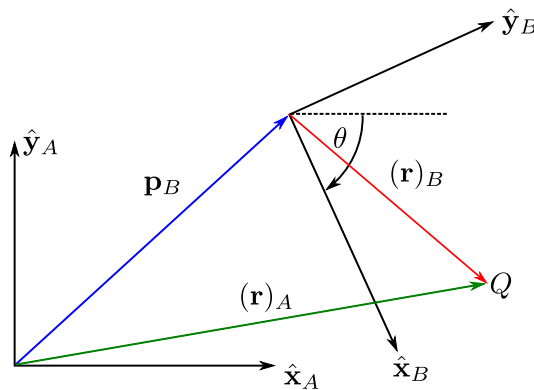


Figure 8: An example of a transformation matrix

Let $(\mathbf{p}_B)_A$ be the position of the origin of the F_B frame relative to the F_A frame, and let \mathbf{R}_B^A be the rotation matrix that describes how F_B is oriented relative to F_A . Then we have the necessary mathematical machinery to formally define a reference frame as a set of two objects:

$$F_B = \{ \mathbf{R}_B^A, (\mathbf{p}_B)_A \} \quad (10)$$

In this definition, the F_A frame is not necessarily the universal F_U frame but it must be uniquely defined

in relation to the F_U frame. (For example, the F_A frame itself may be defined relative to the F_U frame.) To account for the fact that a position vector measured from F_B has a different start point than one that is measured in F_A we must add the difference when mapping between reference frames to obtain the rigid transformation

$$(\mathbf{r})_A = \underbrace{(\mathbf{R})_B^A(\mathbf{r})_B}_{\text{rotating}} + \underbrace{(\mathbf{p}_B)_A}_{\text{translating}} \quad (11)$$

Although Eq. 11 seems quite simple it can become complicated when we have many intermediate reference frames that we are converting from. A simpler representation is to represent Eq. 11 with a single *transformation matrix*, \mathbf{T}_B^A that accounts for both translation and rotation so that

$$(\mathbf{r})_A = \mathbf{T}_B^A(\mathbf{r})_B \quad (12)$$

However, this convenient expression is only possible if we slightly modify how we express our vectors. In particular, we have to use planar *homogeneous coordinates*. With homogeneous coordinates a point $\mathbf{p} = (p_x \ p_y)^T$ is represented by the column vector

$$\mathbf{p} = \begin{pmatrix} p_x \\ p_y \\ 1 \end{pmatrix} \quad (13)$$

The 3rd entry (equal to one) is what makes this a homogeneous coordinate and what makes it possible to represent translations through matrix multiplication. To avoid special notation we assume that it is apparent from context whether the vector is a homogeneous coordinate. Normally, if there are two planar vectors, \mathbf{a} and \mathbf{p} , then we add them as follows

$$\mathbf{a} + \mathbf{p} = \begin{pmatrix} a_1 \\ a_2 \end{pmatrix} + \begin{pmatrix} p_x \\ p_y \end{pmatrix} = \begin{pmatrix} a_1 + p_x \\ a_2 + p_y \end{pmatrix} \quad (14)$$

Using homogeneous coordinates, we can “add” the two homogeneous vectors by using matrix multiplication – i.e., there exists a homogeneous translation matrix $\mathbf{T}_{\text{trans}}(\mathbf{p})$ such that

$$\begin{aligned} \mathbf{a} + \mathbf{p} &= \mathbf{T}_{\text{trans}}(\mathbf{p})\mathbf{a} \\ &= \underbrace{\begin{pmatrix} 1 & 0 & p_x \\ 0 & 1 & p_y \\ 0 & 0 & 1 \end{pmatrix}}_{\mathbf{T}_{\text{trans}}(\mathbf{p})} \begin{pmatrix} a_1 \\ a_2 \\ 1 \end{pmatrix} = \begin{pmatrix} (1)a_1 + (0)a_2 + (p_x)1 \\ (0)a_1 + (1)a_2 + (p_y)1 \\ (0)a_1 + (0)a_2 + (1)1 \end{pmatrix} = \begin{pmatrix} a_1 + p_x \\ a_2 + p_y \\ 1 \end{pmatrix} \end{aligned} \quad (15)$$

Note that Eq. 14 and Eq. 15 produce the same result, except that the result in Eq. 15 is a homogeneous coordinate. Transformation matrices are especially useful because they can combine both rotations *and* translations into one matrix operation and thus they can express rigid vector transformations.

Recall our example in which the reference frame F_B is given in relation to reference frame F_A by \mathbf{R}_B^A and $(\mathbf{p}_B)_A = ((p_{B_x})_A \ (p_{B_y})_A)^T$. We can convert vectors from the F_B frame to the F_A frame using the following transformation matrix

$$\mathbf{T}_B^A = \begin{pmatrix} \cos \theta & -\sin \theta & (p_{B_x})_A \\ \sin \theta & \cos \theta & (p_{B_y})_A \\ 0 & 0 & 1 \end{pmatrix} \quad (16)$$

Note that the 2 x 2 upper left matrix is exactly equal to \mathbf{R}_B^A .

Example: 2D Transformation Matrices

Refer back to Fig. 8. Suppose that the F_B frame is rotated by an angle $\theta = -60^\circ$ relative to $\hat{\mathbf{x}}_A$. The position of a point Q is expressed in the F_B frame in homogenous coordinates is

$$(\mathbf{r})_B = \begin{pmatrix} (r_x)_B \\ (r_y)_B \\ 1 \end{pmatrix} = \begin{pmatrix} 3 \\ 1 \\ 1 \end{pmatrix}$$

The origin of the F_B frame relative to the origin of the F_A frame (and expressed in the F_A frame) is

$$(\mathbf{p}_B)_A = \begin{pmatrix} (p_{B_x})_A \\ (p_{B_y})_A \\ 1 \end{pmatrix} = \begin{pmatrix} 4 \\ 4 \\ 1 \end{pmatrix}$$

To compute the position of the point Q in the F_A frame we use Eqs. 12 and 16.

$$\begin{aligned} (\mathbf{r})_A &= \mathbf{T}_B^A(\mathbf{r})_B \\ &= \begin{pmatrix} \cos(-60^\circ) & -\sin(-60^\circ) & 4 \\ \sin(-60^\circ) & \cos(-60^\circ) & 4 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 3 \\ 1 \\ 1 \end{pmatrix} \\ &= \begin{pmatrix} 0.500 & 0.866 & 4 \\ -0.866 & 0.500 & 4 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 3 \\ 1 \\ 1 \end{pmatrix} \\ &= \begin{pmatrix} 6.366 \\ 1.902 \\ 1 \end{pmatrix} \end{aligned}$$

Compound Transformation Matrices

The power of this formulation is that we can combine multiple rigid transformations into a single matrix. Consider the series of reference frames shown in Fig. 9. Suppose that the position and orientation of each

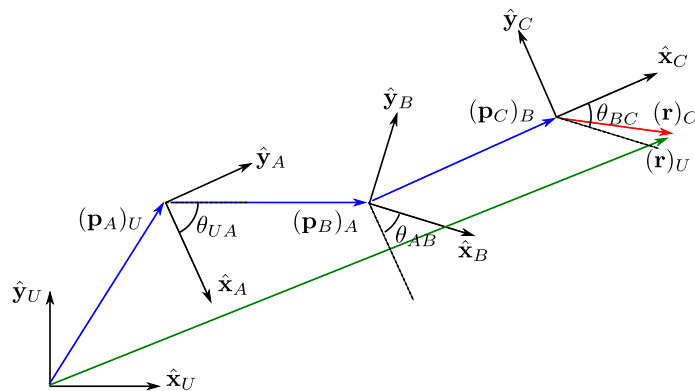


Figure 9: A series of rigid transformations

reference frame's origin is known relative to the position of the previous one and that we may compute \mathbf{T}_A^U , \mathbf{T}_B^A and \mathbf{T}_C^B . Then to convert $(\mathbf{r})_C$ into $(\mathbf{r})_U$ we work our way through all of the intermediate frames, beginning with the conversion from F_C to F_B

$$(\mathbf{r})_B = \mathbf{T}_C^B(\mathbf{r})_C \quad (17)$$

then from F_B to F_A

$$(\mathbf{r})_A = \mathbf{T}_B^A(\mathbf{r})_B \quad (18)$$

and finally from F_A to F_U

$$(\mathbf{r})_U = \mathbf{T}_A^U(\mathbf{r})_A \quad (19)$$

If we substitute Eqs. 17 and 18 into Eq.19 we obtain:

$$\begin{aligned} (\mathbf{r})_U &= \mathbf{T}_A^U(\mathbf{r})_A \\ (\mathbf{r})_U &= \mathbf{T}_A^U[\mathbf{T}_B^A(\mathbf{r})_B] \\ (\mathbf{r})_U &= \mathbf{T}_A^U[\mathbf{T}_B^A[\mathbf{T}_C^B(\mathbf{r})_C]] \\ (\mathbf{r})_U &= \underbrace{(\mathbf{T}_A^U \mathbf{T}_B^A \mathbf{T}_C^B)}_{\mathbf{T}_C^U}(\mathbf{r})_C \end{aligned}$$

The three inner transformation matrices multiple to give a conversion from F_C to F_U thus $\mathbf{T}_A^U \mathbf{T}_B^A \mathbf{T}_C^B = \mathbf{T}_C^U$. Similarly, any number of rigid transformations can be combined. This is a very elegant and compact way of expressing a compound rigid transformation.

Example: Compound Transformation Matrices

Let's return to the example in Fig. 9. In the previous discussion we assumed that \mathbf{T}_A^U , \mathbf{T}_B^A and \mathbf{T}_C^B were given. Suppose that the relative position of each frame $(\mathbf{p}_C)_B$, $(\mathbf{p}_B)_A$ and $(\mathbf{p}_A)_U$ is known and that the angle of each frame *relative to the previous one* is also given as shown in Fig. 9. Specifically, assume the following data

$$(\mathbf{p}_C)_B = \begin{pmatrix} 2.0479 \\ 1.4339 \\ 1 \end{pmatrix} \quad (\mathbf{p}_B)_A = \begin{pmatrix} 1.5000 \\ 2.5981 \\ 1 \end{pmatrix} \quad (\mathbf{p}_A)_U = \begin{pmatrix} 1.5000 \\ 2.5981 \\ 1 \end{pmatrix}$$

and the relative angles are $\theta_{UA} = -60^\circ$, $\theta_{AB} = 45^\circ$, and $\theta_{BC} = 40^\circ$. Note that $(\mathbf{p}_B)_A$ and $(\mathbf{p}_A)_U$ are numerically the same but they point in different directions because they are expressed in different reference frames. The position vector in the F_C frame is

$$(\mathbf{r})_C = \begin{pmatrix} 0.8 \\ -0.6 \\ 1 \end{pmatrix}$$

We wish to express this vector in the F_U frame. We will begin by working our way backwards from the F_C frame, to the F_B frame, to the F_A frame, and finally to the F_U frame. Beginning with the transformation from the F_C frame to the F_B frame, the relative angle is $\theta_{BC} = 40^\circ$ and using $(\mathbf{p}_C)_B$

given above the transformation matrix is

$$\mathbf{T}_C^B = \begin{pmatrix} \cos(40^\circ) & -\sin(40^\circ) & 2 \\ \sin(40^\circ) & \cos(40^\circ) & 4 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} 0.7660 & -0.6428 & 2.0479 \\ 0.6428 & 0.7660 & 1.4339 \\ 0 & 0 & 1 \end{pmatrix} \quad (20)$$

Similarly, from F_B to F_A we have $\theta_{AB} = 45^\circ$ and with $(\mathbf{p}_B)_A$ we obtain

$$\mathbf{T}_B^A = \begin{pmatrix} \cos(45^\circ) & -\sin(45^\circ) & 1.5000 \\ \sin(45^\circ) & \cos(45^\circ) & 2.5981 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} 0.7071 & -0.7071 & 1.5000 \\ 0.7071 & 0.7071 & 2.5981 \\ 0 & 0 & 1 \end{pmatrix} \quad (21)$$

Lastly, from F_A to F_U we have $\theta_{UA} = -60^\circ$ and with $(\mathbf{p}_A)_U$ we obtain

$$\mathbf{T}_A^U = \begin{pmatrix} \cos(-60^\circ) & -\sin(-60^\circ) & 1.5000 \\ \sin(-60^\circ) & \cos(-60^\circ) & 2.5981 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} 0.5000 & 0.8660 & 1.5000 \\ -0.8660 & 0.5000 & 2.5981 \\ 0 & 0 & 1 \end{pmatrix} \quad (22)$$

The compound transformation matrix is

$$\begin{aligned} \mathbf{T}_C^U &= \mathbf{T}_A^U \mathbf{T}_B^A \mathbf{T}_C^B \\ &= \begin{pmatrix} 0.7660 & -0.6428 & 2.0479 \\ 0.6428 & 0.7660 & 1.4339 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 0.7071 & -0.7071 & 1.5000 \\ 0.7071 & 0.7071 & 2.5981 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 0.5000 & 0.8660 & 1.5000 \\ -0.8660 & 0.5000 & 2.5981 \\ 0 & 0 & 1 \end{pmatrix} \\ &= \begin{pmatrix} 0.9063 & -0.4226 & 6.8492 \\ 0.4226 & 0.9063 & 3.4531 \\ 0 & 0 & 1 \end{pmatrix} \end{aligned}$$

and the desired vector in the F_U frame is

$$\begin{aligned} (\mathbf{r})_U &= \mathbf{T}_C^U (\mathbf{r})_C \\ &= \begin{pmatrix} 0.9063 & -0.4226 & 6.8492 \\ 0.4226 & 0.9063 & 3.4531 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 0.8 \\ -0.6 \\ 1 \end{pmatrix} \\ &= \begin{pmatrix} 7.8278 \\ 3.2474 \\ 1 \end{pmatrix} \end{aligned}$$

References

- [1] J. J. Craig. *Introduction to Robotics: Mechanics and Control*. Addison-Wesley, 1989.